

## Can the Esophageal Doppler Monitor Be Used to Clinically Evaluate Peak Left Ventricle $dP/dt$ ?

GLEN M. ATLAS\*

The esophageal Doppler monitor (EDM) is minimally invasive and allows for rapid and continuous cardiovascular measurements which are based upon aortic blood flow characteristics. Using a model derived from the modified Bernoulli equation, a measure of peak left ventricle (PLV)  $dP/dt$  has been developed which utilizes EDM-based parameters:  $PLV \frac{dP}{dt} \propto \frac{V_p^2 \cdot \sqrt{HR}}{T_{FC}}$ ; where  $V_p$  represents peak velocity of aortic blood flow,  $T_{FC}$  is corrected flow time, and HR is heart rate. Additional clinical research is necessary to provide a correlation of this formula with invasive measurements. A wave transmission model of PLV  $dP/dt$  has also been examined. This model requires simultaneous measurement of aortic pulse wave velocity, or aortic flow wave velocity, in order to calculate PLV  $dP/dt$ . Current echocardiographic analyses of PLV  $dP/dt$  show that the wave transmission model provides better correlation with in vivo catheterization results when compared with the modified Bernoulli equation. The EDM remains a useful tool for rapid and continuous evaluation of cardiovascular indices. Further research and development, of this monitor for PLV  $dP/dt$  assessment, is warranted.

**Key words:** esophageal Doppler monitor;  $dP/dt$ ; aortic pulse wave velocity; aortic flow wave velocity.

### INTRODUCTION

It is frequently useful to know peak left ventricle (PLV)  $dP/dt$  for patients with aortic dissections as well as those undergoing aortic reconstructive surgery. Propagation of aortic dissections has been shown to be a function of  $dP/dt$  (Carney *et al.*, 1975; Prokop *et al.*, 1970).

In addition,  $dP/dt$  may be a useful cardiac index as well (Schertel, 1998).

Using only continuous wave Doppler ultrasound, PLV  $dP/dt$  has been shown to correlate with peak aortic blood flow velocity and acceleration (Bargiggia *et al.*, 1989; Hunt *et al.*, 1991; Saeian *et al.*, 1990). PLV  $dP/dt$  has also been successfully derived using a combination of aortic pulse wave velocity and Doppler ultrasound measurements (Senda *et al.*, 1992; Sugawara *et al.*, 1994). These physical models are based either upon the modified Bernoulli equation or a wave transmission model and are reviewed in Appendixes A and B respectively.

Table 1 summarizes the results of several human studies in which PLV  $dP/dt$  was determined noninvasively from aortic blood flow characteristics and then simultaneously compared to left ventricle cardiac catheterization data.

An esophageal Doppler monitor (EDM) has several advantages over traditional ultrasound devices in that it is less expensive, easier to use, and offers continuous real-time measurement of both peak velocity and mean acceleration of descending aortic blood flow (Singer, 1993). Furthermore, the EDM probe can easily be placed orally and used without difficulty with intubated patients who are anesthetized or sedated. Nasal placement, in awake patients, has also been described (Atlas and Mort, 2001).

This device, with its ability to readily measure aortic blood flow indices, would then seem to be potentially useful in minimally-invasive clinical PLV  $dP/dt$  evaluation.

### DERIVATION

Using only continuous wave transthoracic Doppler ultrasound, PLV  $dP/dt$  has been shown to correlate with

\*Department of Anesthesiology, University of Medicine and Dentistry of New Jersey, New Jersey Medical School, 185 S. Orange Avenue, MSB E-538, Newark, New Jersey 07103. E-mail: atlasgm@umdnj.edu

**Table 1. Various Methods Have Been Used to Noninvasively Determine Peak Left Ventricle  $dP/dt$  from Aortic Blood Flow Characteristics**

Correlation with PLV $dP/dt$	Physical model	Reference	Correlation coefficient <sup>a</sup>	Notes <sup>b</sup>
Peak aortic blood flow velocity ( $V_p$ )	$V_p \propto \text{PLV} \frac{dP}{dt}$	Hunt <i>et al.</i> , 1991	0.70	(1)
Mean aortic blood flow acceleration $\frac{V_p^2}{T}$	$\text{AVG}(\frac{dV}{dt}) \propto \text{PLV} \frac{dP}{dt}$	Hunt <i>et al.</i> , 1991	0.75	(2, 3)
	Modified Bernoulli	Hunt <i>et al.</i> , 1991	0.77	(1)
$\frac{dP}{dt} = \rho \cdot V_{pw} \cdot \frac{dV}{dt}$	Wave transmission	Senda <i>et al.</i> , 1992; Sugawara <i>et al.</i> , 1994	0.83; 0.84	(3)

<sup>a</sup>The correlation coefficients are based upon comparisons with in vivo catheterization results.

<sup>b</sup>(1)  $V_p$  is peak aortic blood flow velocity and  $T$  is the time from the start of systole until peak velocity. See Figs. 1 and 2; (2) Mean aortic blood flow acceleration is determined from the start of systole until peak velocity. See Figs. 1 and 2; (3)  $\rho$  represents blood density and  $V_{pw}$  is aortic pulse wave velocity.  $dV/dt$  is acceleration of aortic blood flow.

peak aortic blood flow velocity ( $V_p$ ) by the following formula (Hunt *et al.*, 1991):

$$\text{PLV} \frac{dP}{dt} \propto \frac{V_p^2}{T} \quad (1)$$

where  $T$  represents the time from the onset of aortic blood flow until it reaches peak velocity  $V_p$ . It should be noted that Eq. (1) represents an approximation of the first derivative, with respect to time, of the modified Bernoulli equation. This is described in Appendix A.

Figure 1 illustrates the relationship between  $V_p$  and  $T$  for a representative EDM-derived aortic Doppler signal. Hunt *et al.* (1991) showed good correlation of  $\frac{V_p^2}{T}$  to PLV  $dP/dt$  and only slightly less correlation of  $V_p$  and mean acceleration to PLV  $dP/dt$ . These results are summarized in Table 1 (see Figs. 1 and 2).

Therefore, the ease of measuring  $V_p$  and mean acceleration, in real-time with current EDM technology, would make either of these clinically appealing “markers” for quickly assessing PLV  $dP/dt$  at the bedside.

Corrected flow time,  $T_{FC}$ , ordinarily correlates with preload and is readily determined with the EDM. The relationship between cycle time and flow time,  $T_F$ , is shown in Fig. 1. Equation (2) defines  $T_{FC}$ , utilizing  $T_F$ , and is based upon a modification of Bazett’s equation:

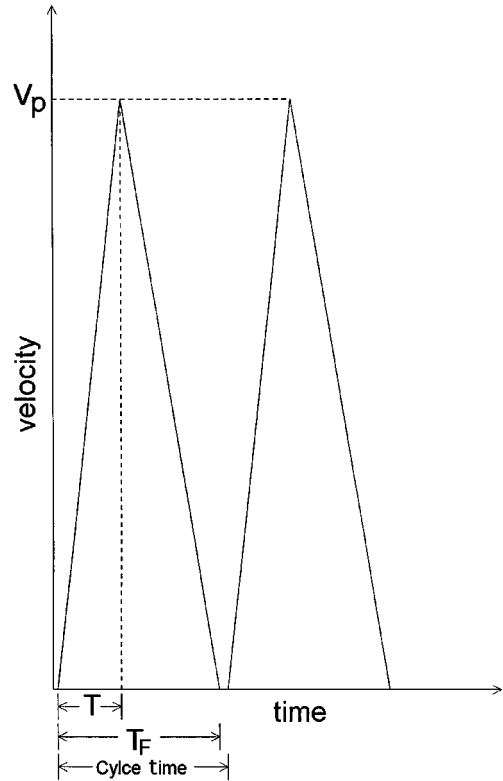
$$T_{FC} = \frac{T_F}{\sqrt{\text{Cycle time}}} \quad (2)$$

Cycle time is equivalent to RR interval and is related to heart rate, HR, as shown below:

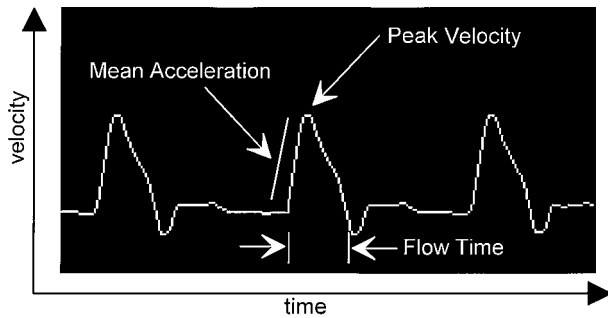
$$\text{Cycle time} = \text{RR interval} = \frac{60}{\text{HR}} \quad (3)$$

where HR is expressed in beats per minute and cycle time, as well as RR interval, are expressed in seconds. In addition, the time to peak velocity,  $T$ , and flow time,  $T_F$ , are related:

$$T \approx \frac{T_F}{2} \quad (4)$$



**Figure 1.** This diagram illustrates the aortic blood flow velocity vs. time relationship. The EDM is a minimally-invasive device which is able to measure this accurately and in real time.  $T$  represents time until peak velocity and  $T_F$  is flow time or left ventricle ejection time.



**Figure 2.** Typically EDM waveform. Mean acceleration is the average slope of aortic blood flow velocity from onset of systole until peak velocity. Flow time represents left ventricle ejection time.

Eqs. (2)–(4) can be substituted into Eq. 1 to yield the following:

$$\text{PLV} \frac{dP}{dt} \propto \frac{V_P^2 \cdot \sqrt{\text{HR}}}{T_{\text{FC}}} \quad (5)$$

Thus, based on Eq. (5), it would seem that the EDM could provide a useful real-time assessment of PLV  $dP/dt$  using a model similar to that of Hunt *et al.* (1991).

By combining simultaneous pulse wave velocity measurement with aortic Doppler ultrasound, excellent correlations, of derived-to-measured PLV  $dP/dt$ , have also been obtained (Senda *et al.*, 1992; Sugawara *et al.*, 1994). This has been accomplished with the use of a wave transmission model in which PLV  $dP/dt$  is determined with the following equation of continuity (see Appendix B):

$$\frac{dP}{dt} = \rho \cdot V_{\text{pw}} \cdot \frac{dV}{dt} \quad (6)$$

where  $\rho$  represents blood density,  $V_{\text{pw}}$  is aortic pulse wave velocity, and  $dV/dt$  is acceleration of aortic blood flow.

## DISCUSSION

Given the clinical benefit of the EDM for safe and rapid assessment of cardiovascular parameters, it would seem reasonable to evaluate this device for its usefulness as a minimally-invasive tool for bedside evaluation of PLV  $dP/dt$ . Pharmacological management of aortic dissections, as well as other aortic injuries, could then potentially be improved.

Currently, labetalol, a combination nonspecific  $\beta$  blocker and  $\alpha$  blocker, remains the treatment of choice for hemodynamic control of patients with aortic dissec-

tions (Grubb *et al.*, 1987). Esmolol, an ultra-short acting  $\beta$  blocker, has also been reported as useful (O’Conner and Luntley, 1995). Therefore, the utility of these agents could possibly be evaluated, in real-time, with EDM-based measurements of PLV  $dP/dt$ .

Using existing EDM technology, clinical results, based on Eq. (5), would seem easily comparable with simultaneously obtained measurements from in vivo catheterization.

It is important to realize that  $dP/dt$  can be modeled, with Eq. (6), as a function that is based upon aortic pulse wave velocity. This has been substantiated using the wave transmission model by Senda *et al.*, 1992 and Sugawara *et al.*, 1994. With this model, they have demonstrated excellent correlations of PLV  $dP/dt$  directly to catheterization results.

The clinical utility of aortic pulse wave velocity has been investigated. As shown in Appendix B, aortic  $V_{\text{pw}}$  is inversely associated with aortic compliance (Lehmann, 1999). In subjects over 70 years old, aortic pulse wave velocity was found to be a marker of cardiovascular disease (Meaume *et al.*, 2001). In hemodialysis patients, an increased  $V_{\text{pw}}$  has been shown to be an independent predictor of both all-cause and cardiovascular mortality (Blacher *et al.*, 1999a).  $V_{\text{pw}}$  has also been shown to increase with atherosclerotic disease (Blacher *et al.*, 1999b; Hopkins *et al.*, 1994; Lehmann, 1999). Furthermore, in Marfan syndrome patients,  $\beta$  blocker therapy has been shown to decrease aortic  $V_{\text{pw}}$  (Groenink *et al.*, 1998).

It should be noted that typical values for aortic  $V_{\text{pw}}$ , in humans, range from 3 to 10  $\text{M} \cdot \text{s}^{-1}$ . In addition,  $V_{\text{pw}}$  normally increases with age (Bulpitt *et al.*, 1999; Rogers *et al.*, 2001).

Therefore,  $V_{\text{pw}}$  appears to be a clinically useful marker of aortic compliance. The wave transmission model of  $dP/dt$  takes this parameter into account in contrast to models based upon the modified Bernoulli equation.

If the effects of reflected waves are assumed to be negligible, then aortic flow wave velocity and pulse wave velocity would be identical. It should be noted that aortic flow wave velocity,  $V_{\text{fw}}$ , has also been investigated using magnetic resonance imaging. Age-related values for  $V_{\text{fw}}$ , that are similar to those for  $V_{\text{pw}}$ , were found. In addition, values of  $V_{\text{fw}}$  were shown to inversely correlate with those of aortic compliance (Kraft *et al.*, 2001; Mohiaddin *et al.*, 1993).

Thus, using the wave transmission model, it may be reasonable to correlate aortic flow wave velocity with aortic pulse wave velocity in noninvasive, or minimally-invasive, determinations of PLV  $dP/dt$ .

## SUMMARY

Therefore, the EDM may provide a useful means of assessing PLV  $dP/dt$ . This could easily be accomplished with existing EDM indices. Currently, there is no readily-available instrument that allows for simple and rapid bedside determination of PLV  $dP/dt$ .

Clearly, this information could potentially provide the clinician with an improved ability to care for patients with aortic dissections and related injuries. The use of PLV  $dP/dt$ , as a cardiac index, would also be valuable.

It should also be remembered that a clinically useful guide to “gauging” PLV  $dP/dt$  may be obtained from simply observing the peak velocity, or mean acceleration, of aortic blood flow.

Further studies are warranted to correlated EDM-derived aortic  $dP/dt$  data with in vivo catheterization results. In addition, future means of assessing PLV  $dP/dt$  could possibly include simultaneous measurement of aortic pulse wave velocity.

Determination of aortic flow wave velocity, and its correlation with aortic pulse wave velocity, may also facilitate real-time PLV  $dP/dt$  evaluation.

## APPENDIX A: MODIFIED BERNOULLI EQUATION

The Bernoulli equation states that hydraulic pressure,  $P$ , is the sum of ambient pressure, kinetic energy per unit volume, and hydrostatic pressure (Milnor, 1982):

$$P = P_a + \frac{1}{2}\rho v^2 + \rho gh \quad (1A)$$

where  $P_a$  is ambient pressure,  $\rho$  is blood density,  $v$  is the velocity of aortic blood flow, and  $g$  and  $h$  are acceleration due to gravity and height respectively. These effects are neglected in the modified Bernoulli equation:

$$P = \frac{1}{2}\rho v^2 \quad (2A)$$

$P_a$  and  $\rho gh$  are both time-invariant and therefore:

$$\frac{d}{dt}(P_a) = 0 \quad \text{and} \quad \frac{d}{dt}(\rho gh) = 0 \quad (3A)$$

Thus

$$\frac{dP}{dt} = \frac{d}{dt} \left( \frac{1}{2}\rho v^2 \right) \quad (4A)$$

With  $T$  being the time until peak velocity,  $V_p$ :

$$\text{PLV} \frac{dP}{dt} \approx \frac{\frac{1}{2}\rho V_p^2}{T} \quad (5A)$$

Thus

$$\text{PLV} \frac{dP}{dt} \propto \frac{V_p^2}{T} \quad (6A)$$

## APPENDIX B: WAVE TRANSMISSION MODEL

As described in Appendix C, the wave transmission model is based upon the following equation of continuity:

$$\frac{dP}{dt} = \rho \cdot V_{pw}^2 \cdot \frac{dV}{dx} \quad (1B)$$

It should be noted that:

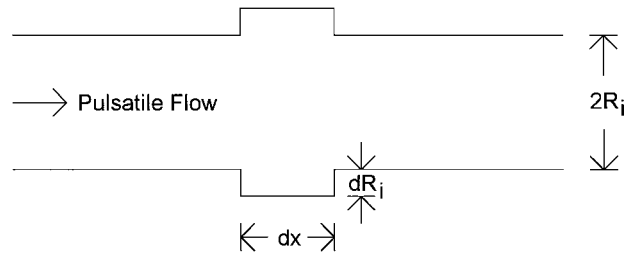
$$V_{pw}^2 = \left( \frac{dx}{dt} \right)^2 \quad (2B)$$

The propagation of  $dx/dt$ , which is pulse wave velocity,  $V_{pw}$ , is illustrated in Fig. 3. Substituting (2B) into (1B) yields:

$$\frac{dP}{dt} = \rho \cdot \left( \frac{dx}{dt} \right)^2 \cdot \frac{dV}{dx} = \rho \cdot \left( \frac{dx}{dt} \right) \cdot \frac{dV}{dt} \quad (3B)$$

Thus

$$\frac{dP}{dt} = \rho \cdot V_{pw} \cdot \frac{dV}{dt} \quad (4B)$$



**Figure 3.** Pulsatile flow, in a distensible vessel, generates a pulse wave  $dx$ . The velocity of the pulse wave,  $V_{pw}$ , is equal to  $dx/dt$  and is a function of the stiffness of the vessel and its geometry (Milnor, 1982).

$V_{pw}$  has been described, based on physical parameters, with the Moens–Korteweg equation:

$$V_{pw} = \sqrt{\frac{E \cdot h}{2 \cdot \rho \cdot R_i}} \quad (5B)$$

where  $E$  represents Young's modulus which increases as vessel wall stiffness increases. The width of the vessel wall is denoted as  $h$  and its internal radius is  $R_i$ .

The Moens–Korteweg equation (5B) can also be expressed based on compliance  $C = \frac{d(\text{Vol})}{dP}$  and total vessel volume (Vol):

$$V_{pw} = \sqrt{\frac{dP \cdot (\text{Vol})}{\rho \cdot d(\text{Vol})}} = \sqrt{\frac{(\text{Vol})}{\rho \cdot C}} \quad (6B)$$

Thus, pulse wave velocity is inversely proportional to the square root of compliance (Milnor, 1982).

### APPENDIX C: DERIVATION OF THE EQUATION OF CONTINUITY

Utilizing Fig. 3, the equation of continuity, Eq. (1B), can be derived (Milnor, 1982) based upon the assumption that:

$$\frac{dQ}{dx} \Big|_{\text{radial}} = \frac{dQ}{dx} \Big|_{\text{axial}} \quad (1C)$$

$$\frac{dQ}{dx} \Big|_{\text{radial}} = \left( \frac{d(\text{vol})}{dt} \right) \frac{d}{dx} = \frac{d}{dt} (\pi R_i^2) \quad (2C)$$

Thus

$$\frac{dQ}{dx} \Big|_{\text{radial}} = 2\pi R_i \frac{dR_i}{dt} \quad (3C)$$

For flow in the axial direction,  $Q = (\text{area}) \cdot (\text{velocity})$  and therefore:

$$\frac{dQ}{dx} \Big|_{\text{axial}} = (\pi R_i^2) \frac{dV}{dx} \quad (4C)$$

Equations (3C) and (4C) can be substituted into (1C) to yield:

$$2\pi R_i \frac{dR_i}{dt} = (\pi R_i^2) \frac{dV}{dx} \quad (5C)$$

Rearranging

$$\frac{dR_i}{dt} = \frac{R_i}{2} \cdot \frac{dV}{dx} \quad (6C)$$

Young's modulus is defined as  $E = \frac{\text{stress}}{\text{strain}}$ , where strain =  $\frac{dR_i}{R_i}$ . Stress can then be defined as:

$$\text{stress} = \frac{R_i \cdot dP}{h} \quad (7C)$$

where  $h$  represents vessel wall thickness.

By substitution, Young's modulus is then:

$$E = \frac{R_i \cdot dP}{h} \cdot \frac{R_i}{dR_i} \quad (8C)$$

Rearranging,  $dR_i$  can then be expressed as:

$$dR_i = \frac{R_i \cdot dP}{h} \cdot \frac{R_i}{E} \quad (9C)$$

Substituting Eq. (9C) into Eq. (6C) yields:

$$\left( \frac{R_i \cdot dP}{h} \cdot \frac{R_i}{E} \right) \frac{dV}{dx} = \frac{R_i}{2} \cdot \frac{dV}{dx} \quad (10C)$$

Rearranging Eq. (10C) yields:

$$\frac{dP}{dt} = \frac{E \cdot h}{2 \cdot R_i} \cdot \frac{dV}{dx} \quad (11C)$$

The following is the Moens–Korteweg equation for pulse wave velocity:

$$\left( \frac{dx}{dt} \right)^2 = V_{pw}^2 = \frac{E \cdot h}{2 \cdot \rho \cdot R_i} \quad (12C)$$

The equation of continuity can be expressed by substituting Eq. (12C) into (11C):

$$\frac{dP}{dt} = \rho \cdot V_{pw}^2 \cdot \frac{dV}{dx} \quad (13C)$$

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